

Appendix G: Answers to Even-Numbered Problems

Unless stated otherwise, x components are positive to the right, y components are positive upward, and counterclockwise moments are positive.

1.2	$A_x = 0, A_y = 2.5 \text{ kN}, B = 27.5 \text{ kN}.$
1.4	$A = 35 \text{ lb}, B = 25 \text{ lb}.$
1.6	$P = 0, V = -144 \text{ kN}, M = -288 \text{ kN}\cdot\text{m}.$
1.8	$\mathbf{R} = 173\mathbf{i} + 100\mathbf{j} \text{ (N)}, \mathbf{M} = -396\mathbf{k} \text{ (N}\cdot\text{m)}.$
1.10	$m = 52.3 \text{ kg}.$
1.12	84.9 kN (T)
1.14	$F = 2.48 \text{ kip}.$
1.16	Member CE , 4.72 kN (T) . Member DE , 3.92 kN (C)
1.18	$AC : 150 \text{ kN (T)}, BC : 90.1 \text{ kN (T)}, BD : 225 \text{ kN (C)}.$
1.20	$C_x = 0, C_y = F, D_x = 0, D_y = -2F, E = F.$
1.22	$3876 \text{ lb. (compression)}$
1.24	$6000 \text{ lb. (tension)}$
1.26	$1.70 \text{ kN (tension)}$
1.28	$1.65 \text{ kN (compression)}$
1.30	$A_x = 15 \text{ kN}, A_y = -8 \text{ kN}, E_x = -15 \text{ kN}, E_y = 14 \text{ kN}.$
1.32	$\bar{x} = 667 \text{ mm}, \bar{y} = 133 \text{ mm}.$
1.34	$\bar{x} = 90.3 \text{ mm}, \bar{y} = 59.4 \text{ mm}.$
1.36	Distance $= 3.28 \text{ ft}.$
1.38	(a) $A_x = 0, A_y = 80.7 \text{ N}, B = 210 \text{ N}.$ (b) $w = 223 \text{ N/m}.$
1.40	$A_x = 0, A_y = 159 \text{ lb}, B = 169 \text{ lb}.$
1.42	$R_x = 0, R_y = -913 \text{ N}, M_R = 1970 \text{ N}\cdot\text{m}$ clockwise
1.46	$A = c_0/2, B_x = 0, B_y = -c_0/2.$
2.2	(a) $A' = 0.00354 \text{ m}^2.$ (b) $\sigma_{av} = 1.20\text{E}6 \text{ Pa}, \tau_{av} = 1.20\text{E}6 \text{ Pa}.$
2.4	(a) $\sigma_{av} = 318 \text{ psi}.$ (b) $\sigma_{av} = -637 \text{ psi}.$
2.6	$P = 8.18 \text{ kN}, \tau_{av} = -168 \text{ kPa}.$
2.8	$\sigma_{av} = 267 \text{ psi}, \tau_{av} = 533 \text{ psi}.$
2.10	$\sigma_{av} = 20,400 \text{ psi}.$

2.12	$\sigma_{av} = 74.6x \text{ kPa. } (x \text{ in meters})$
2.14	$\sigma_{av} = 22.8 \text{ psi, } \tau_{av} = 62.6 \text{ psi.}$
2.16	$\sigma_{av} = 200 \text{ kPa, } \tau_{av} = 83.3 \text{ kPa.}$
2.18	$\sigma_{av} = 5.96 \text{ MPa (864 psi).}$
2.20	(a) $\sigma_{av} = 9.42 \text{ MPa. (b)}$ $\sigma_{av} = 13.3 \text{ MPa.}$
2.22	(a) $\tau_{av} = P/A. \text{ (b)}$ $\tau_{av} = P/(2A).$
2.24	$\tau_{av} = 41.7 \text{ MPa.}$
2.26	$\sigma_{av} = 102 \text{ ksf.}$
2.28	$ \tau_{av} = 3.60 \text{ ksi.}$
2.30	$\sigma_{av} = 31.1 \text{ MPa, } \tau_{av} = 9.17 \text{ MPa.}$
2.32	$\sigma_{av} = -129 \text{ psi, } \tau_{av} = 153 \text{ psi.}$
2.34	$\tau_{av} = 18.75 \text{ psi.}$
2.36	$\tau_{av} = 21.2 \text{ MPa.}$
2.38	$\tau_{av} = F/(bt).$
2.40	$\tau_{av} = 1.82 \text{ psi.}$
2.42	$\sigma = 50 \text{ kPa.}$
2.44	$\sigma = 2860 \text{ psi.}$
2.46	(a) $70\mathbf{i} - 10\mathbf{j} - 5\mathbf{k} \text{ (kN). (b)}$ $-70\mathbf{i} + 10\mathbf{j} + 5\mathbf{k} \text{ (kN).}$
2.48	$\sigma_{av} = 0.533 \text{ MPa.}$
2.50	$\mathbf{t}_{av} = 1.955\mathbf{i} + 0.090\mathbf{j} + 1.060\mathbf{k} \text{ (MPa).}$
2.52	$a = 111 \text{ lb/in}^3.$
2.54	$dL' = 1.15dL.$
2.56	$L' = 6.24 \text{ in.}$
2.58	$L' = 0.2113 \text{ m.}$
2.60	$\epsilon = 0.00625.$
2.62	$\delta = -3.60 \text{ mm.}$
2.64	$\delta = 0.028 \text{ in.}$

(continued)

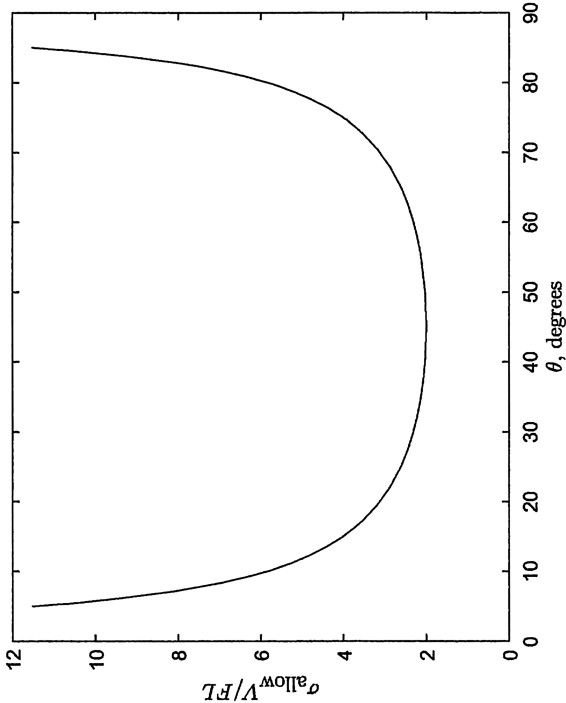
2.66	$\epsilon_{AB} = 0.1062.$
2.68	$\epsilon = 0.00454.$
2.70	$\epsilon = 0.0075.$
2.72	$\epsilon_1 = 0.000333, \epsilon_2 = -0.008333.$
2.74	$\gamma_{12} = 0.698.$
2.76	$\gamma_{12} = 0.0870.$
2.78	$\gamma_{12} = -0.234.$
2.80	$\epsilon_x = 0.00296, \epsilon_y = 0.00204, \epsilon_z = 0.00204, \gamma_{xy} = -0.00370, \gamma_{yz} = 0, \gamma_{xz} = 0.$
2.82	$\sigma_{av} = 0, \tau_{av} = 398 \text{ psi}.$
2.84	$\sigma_{av} = 320 \text{ psi}.$
2.86	$\sigma_{av} = 200 \text{ kPa}, \tau_{av} = 0.$
2.88	$\sigma_{av} = -750 \text{ kPa}.$
2.90	$\sigma_{av} = -500 \text{ kPa}, \tau_{av} = 267 \text{ kPa}.$
2.92	$\tau_{av} = 92.9 \text{ MPa}.$
2.94	$\tau_{av} = 2.32 \text{ MPa}.$
2.96	$L' = 0.2008 \text{ m}.$
2.98	$\delta = -0.028 \text{ in}.$
2.100	$\epsilon = 0.02.$
2.102	$\epsilon = 0.476.$
3.2	(a) $\sigma_{AB} = 2.83 \text{ MPa}.$ (b) $\sigma_{BC} = 0.943 \text{ MPa}.$
3.4	$\sigma = 568 \text{ kPa}.$
3.6	$\sigma = 4.5 \text{ ksi}.$
3.8	$\sigma_{BC} = -578 \text{ MPa}, \sigma_{DG} = 1440 \text{ MPa}.$
3.10	$\sigma = -10.3 \text{ MPa}.$
3.12	$\sigma = 4.90 \text{ ksi}.$
3.16	$\sigma_{BC} = 106 \text{ MPa}.$
3.18	$F = 2170 \text{ N}.$
3.20	$\sigma_\theta = 1.75 \text{ ksi}, \tau_\theta = -4.82 \text{ ksi}.$

3.22	$\theta = 50.2^\circ, P = 61.0 \text{ kN}.$
3.24	(a) $ \tau_\theta = 0.$ (b) $ \tau_\theta = 18.2 \text{ MPa}.$ (c) $ \tau_\theta = 27.9 \text{ MPa}.$
3.26	$F = 5200 \text{ lb}.$
3.28	$F = 173 \text{ kN}.$
3.30	$\sigma_{AB} = -1900 \text{ psi}.$
3.32	$\sigma_3 = -63.1 \text{ MPa}.$
3.34	$10.02 \text{ in}.$
3.36	$\sigma = -0.7 \text{ GPa}.$
3.38	$E = 76.4 \text{ GPa}, \nu = 0.351.$
3.40	57.1 kip
3.42	$\delta_{AB} = 0.107 \text{ in}, \delta_{AC} = -0.0571 \text{ in}.$
3.44	$x = b/(1 + E_{BC}L_{DC}/E_{DC}L_{BC}).$
3.46	$0.01 \text{ in}.$
3.48	$1.95^\circ \text{ clockwise}$
3.50	$\delta_{BE} = 0.0411 \text{ in}.$
3.52	$\delta_{AB} = 5.28 \text{ mm}, \delta_{AC} = -3.96 \text{ mm}.$
3.54	$\delta_{BC} = 0.845 \text{ mm}, \delta_{BD} = 0.602 \text{ mm}.$
3.56	$-0.0199 \text{ mm}.$
3.60	$\sigma = 2F/(3A).$
3.62	$\sigma_{\text{rod}} = -87.0 \text{ MPa}, \sigma_{\text{sleeve}} = -16.0 \text{ MPa}.$
3.64	$\sigma_{BC} = -7.16 \text{ MPa}.$
3.66	$F_1 = 76.2 \text{ kN}.$
3.68	$b = 0.0681 \text{ in}.$
3.70	$\sigma_{AB} = -F\cos^2\theta[A(1 + \cos^3\theta)], \sigma_{AC} = -F/[A(1 + \cos^3\theta)].$
3.72	310 kN
3.74	$h = 2.95 \text{ mm}.$
3.76	$\sigma_{BC} = -72.1 \text{ MPa}, \sigma_{DG} = 126 \text{ MPa}, \sigma_{HI} = 390 \text{ MPa}.$

(continued)

3.78	9.92 kN
3.80	23.5 kN
3.82	0.268 mm to the left, 0.247 mm upward
3.84	$\delta = 0.0116$ in.
3.86	$\delta = 0.392$ mm.
3.88	$\sigma_L = 30.6$ ksi.
3.90	$\delta = 0.127$ mm.
3.92	$\delta = 6.13$ mm.
3.94	$\delta = 0.0588$ m.
3.96	$\delta = 0.0682$ m.
3.98	$x = 1.26$ m, displacement = 0.101 mm.
3.100	$\sigma_A = 57.6$ ksi.
3.102	0.00137 mm
3.104	$\delta = -F/\pi Ed \tan^2 \alpha$.
3.106	$\delta = 0.0131$ mm.
3.108	200.132 mm.
3.110	30.024 mm
3.112	$\sigma = 0$.
3.114	(a, b) $\delta = 0.0111$ in.
3.116	134 °F
3.118	$\sigma = -7470$ psi.
3.120	$\sigma_A = -16.8$ MPa, $\sigma_B = -67.2$ MPa.
3.122	$\sigma_{\text{sleeve}} = -557$ MPa.
3.124	16,000 lb. downward
3.126	0.369 in. to the right, 0.184 in. upward
3.128	1.20 mm to the left, 19.01 mm downward
3.130	$\sigma_{AB} = \sigma_{AD} = 46.3$ MPa, $\sigma_{AC} = 79.8$ MPa.
3.132	$\sigma_{AB} = -96.0$ MPa, $\sigma_{AC} = -109$ MPa.

3.134	0.916 mm
3.136	Either 2014-T6 or 7075-T6
3.138	ASTM-A514
3.140	3.70 in ²
3.142	



3.144	2014-T6 or 7075-T6
3.150	$A = 0.00912 \text{ in}^2$
3.152	$A_3 = 1850 \text{ mm}^2$
3.154	$\sigma_{AB} = 2.31 \text{ MPa}$
3.156	$\sigma_{AB} = 488 \text{ MPa}$, $\sigma_{AC} = 345 \text{ MPa}$

(continued)

3.158	$\sigma = 1.12 \text{ MPa.}$
3.160	$\sigma_\theta = 120.0 \text{ ksi, } \tau_\theta = 69.3 \text{ ksi.}$
3.162	$D' = 0.7495 \text{ in.}$
3.164	$\epsilon_{AB} = 0.000349, \epsilon_{CD} = 0.000698, \epsilon_{EF} = 0.001047.$
3.166	$\delta_{AB} = 0.292 \text{ in, } \delta_{AC} = -0.137 \text{ in.}$
3.168	$A : 400\text{E}6 \text{ N (tension); } B : 400\text{E}6 \text{ N (compression).}$
3.170	$40 \text{ }^\circ\text{C}$
3.172	$\sigma_{AB} = 81.7 \text{ MPa, } \sigma_{AC} = -35.5 \text{ MPa, } \sigma_{AD} = -82.6 \text{ MPa,}$
4.2	$\beta = 89.0^\circ.$
4.4	$\beta = 89.9^\circ.$
4.6	$G = 75.8 \text{ GPa.}$
4.8	$\sigma_\theta = 10.4 \text{ MPa, } \tau_\theta = 6 \text{ MPa.}$
4.10	$\tau = 16.2 \text{ MPa.}$
4.12	(a) $\sigma_\theta = -17.3 \text{ ksi, } \tau_\theta = 10 \text{ ksi. (b) } 20 \text{ ksi}$
4.14	$\tau = 3.97 \text{ MPa, } \theta = 20.5^\circ.$
4.16	$J = 23.6 \text{ in}^4.$
4.18	$ \tau = 17.0 \text{ MPa.}$
4.20	$ \tau = 19.9 \text{ MPa.}$
4.22	$ \tau = 11.7 \text{ MPa.}$
4.24	$ \tau = 31.8 \text{ MPa.}$
4.26	$R_o = 69.5 \text{ mm.}$
4.28	$\phi = 3.96 \text{ rad } (227^\circ).$
4.30	$\phi = 0.000382 \text{ rad } (0.0219^\circ)$
4.32	(a) $ \tau = 637 \text{ psi. (b) } 0.00110 \text{ rad } (0.0629^\circ).$
4.34	$ \tau_{AB} = 19.9 \text{ ksi, } \tau_{BC} = 8.49 \text{ ksi.}$

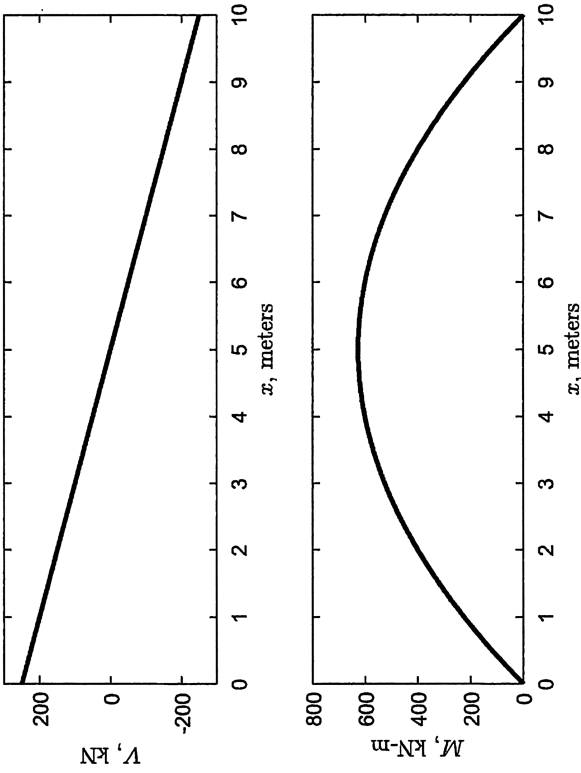
4.36	$ \tau_{AB} = 30.9 \text{ MPa}$, $ \tau_{BC} = 61.8 \text{ MPa}$, $ \tau_{CD} = 124 \text{ MPa}$.
4.38	$ \tau_{AB} = 37.7 \text{ MPa}$, $ \tau_{CD} = 28.3 \text{ MPa}$.
4.40	$r_C = 108 \text{ mm}$.
4.42	$ T_0 = 13.7 \text{ in-kip}$.
4.44	$ T_{AB} = 1110 \text{ N-m}$, $ T_{BC} = 92.3 \text{ N-m}$.
4.46	$\phi = 0.0107 \text{ rad } (0.614^\circ)$.
4.48	$ \phi_A = 1.82^\circ$, $ \phi_B = 0.180^\circ$.
4.50	656 MPa
4.52	$ \tau = 21.9 \text{ MPa}$.
4.54	$ \tau = 17.9 \text{ ksi}$.
4.56	$ \tau = 2.83 \text{ ksi}$.
4.58	$a = 0.251 \text{ m}^{-1}$.
4.60	$T = 6.19 \text{ N-m}$.
4.62	102 N-m
4.64	$ \tau = 40.7 \text{ MPa}$.
4.66	$c_0 = 7200 \text{ in-lb/in.}$, $ \tau = 18.7 \text{ ksi}$.
4.70	$ T_{\text{left}} = 5c_0L/192$, $ T_{\text{right}} = c_0L/64$.
4.72	$T = 6.49 \text{ kN-m}$.
4.74	$\phi = 117^\circ$.
4.76	$r_Y = 0.553 \text{ in}$, $\phi = 74.6^\circ$.
4.78	$T = 15.5 \text{ kN-m}$.
4.80	$\phi = 142^\circ$.
4.84	$\phi = 0.00937 \text{ rad } (0.537^\circ)$.
4.86	(a) $ \tau = 27.8 \text{ MPa}$. (b) $ \tau = 19.4 \text{ MPa}$.
4.88	$ \tau = 30.4 \text{ MPa}$.
4.90	$\phi = 0.975^\circ$.

(continued)

4.92	$ \mathbf{r} = 5540 \text{ psi}$.
4.94	$t = 0.0802 \text{ in}$, $\phi = 1.95^\circ$.
4.96	$\phi = 4.27^\circ$.
4.98	$ \mathbf{r} = 68.5 \text{ MPa}$.
4.100	(a) $ \mathbf{r} = 1591.5 \text{ lb/in}^2$, (b) $ \mathbf{r} = 1590.6 \text{ lb/in}^2$.
4.102	$ \tau_{\max} = 31.8 \text{ MPa}$.
4.104	7075-T6 aluminum alloy
4.116	$G = 1.22\text{E}7 \text{ psi}$.
4.118	$\gamma = 0.00346$.
4.120	$\phi = 0.000668 \text{ rad}$ (0.0383°).
4.122	$T = 1.99 \text{ kN}\cdot\text{m}$.
4.124	$\sigma_\theta = 20.5 \text{ kPa}$, $ \tau_\theta = 24.4 \text{ kPa}$.
4.126	$ \tau_{AB} = 8.13 \text{ ksi}$, $ \tau_{BC} = 4.06 \text{ ksi}$.
4.128	$ \tau = 325 \text{ MPa}$.
5.2	$P_C = 0$, $V_C = -0.5 \text{ kN}$, $M_C = 0.5 \text{ kN}\cdot\text{m}$.
5.4	$P_B = 0$, $V_B = 2 \text{ kN}$, $M_B = -2 \text{ kN}\cdot\text{m}$.
5.6	(b) $A_x = 0$, $A_y = 0$, $B_y = 0$. (c) $P_C = 0$, $V_C = 0$, $M_C = -4 \text{ kN}\cdot\text{m}$.
5.8	(a) $P_A = 0$, $V_A = 4 \text{ kN}$, $M_A = 4 \text{ kN}\cdot\text{m}$. (b) $P_A = 0$, $V_A = 2 \text{ kN}$, $M_A = 3 \text{ kN}\cdot\text{m}$.
5.10	$P_A = 0$, $V_A = 16.7 \text{ lb}$, $M_A = 575 \text{ in}\cdot\text{lb}$.
5.12	$P_A = 0$, $V_A = -475 \text{ lb}$, $M_A = -1275 \text{ ft}\cdot\text{lb}$.
5.14	$P_A = 0$, $V_A = 4.8 \text{ kN}$, $M_A = 13.6 \text{ kN}\cdot\text{m}$.
5.16	$P_C = 0$, $V_C = -3.7 \text{ kN}$, $M_C = 14.1 \text{ kN}\cdot\text{m}$.
5.18	$P_B = 10.7 \text{ kN}$, $V_B = -12 \text{ kN}$, $M_B = 1.4 \text{ kN}\cdot\text{m}$.
5.20	$P_B = 90 \text{ kN}$, $V_B = -40 \text{ kN}$, $M_B = -20 \text{ kN}\cdot\text{m}$.

5.22

(a) $P = 0$, $V = -50x + 250$ kN, $M = -25x^2 + 250x$ kN·m. (c)



5.24

(a) $P = 0$, $V = 1080 - 10x^2$ lb, $M = 1080x - (10/3)x^3$ ft·lb. (c) $M = 7480$ ft·lb at $x = 10.4$ ft.

5.26

$P = 0$, $V = -F$, $M = -Fx$.

5.28

$P = 0$, $V = -20$ N, $M = -20x$ N·m.

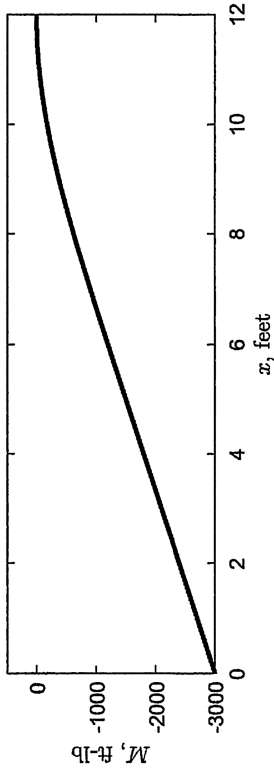
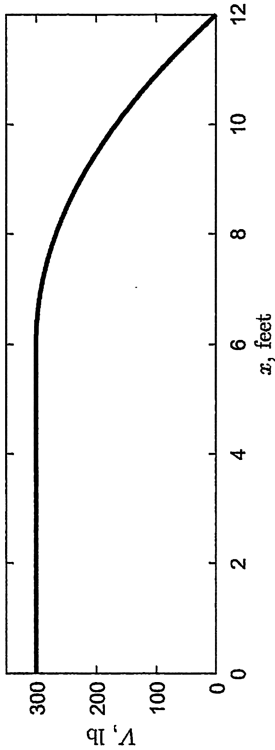
5.30

$P = 0$, $V = -400 - (25/3)x^2$ lb, $M = -400x - (25/9)x^3$ ft·lb.

(continued)

5.32

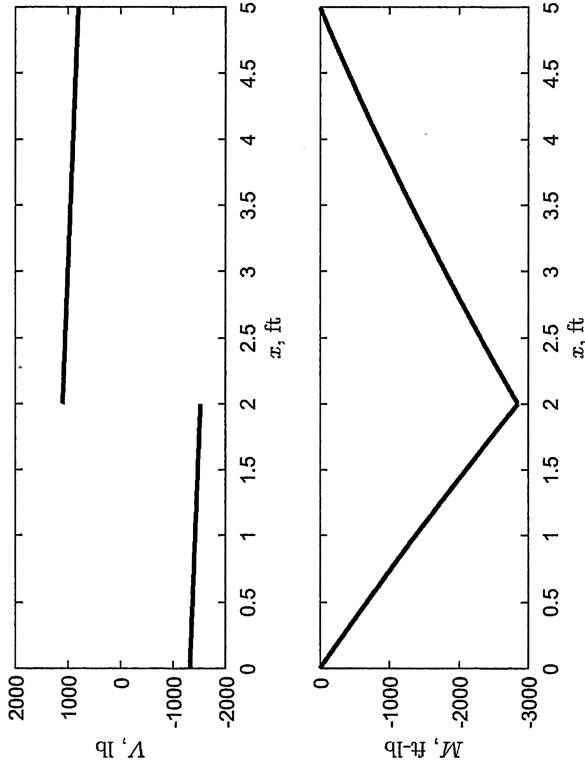
(a) $0 < x < 6$ ft: $P = 0$, $V = 300$ lb, $M = 300x - 3000$ ft-lb, $6 < x < 12$ ft: $P = 0$, $V = 300 - (25/3)(x - 6)^2$ lb, $M = -3000 + 300x - (25/9)(x - 6)^3$ ft-lb.
(b)



5.34

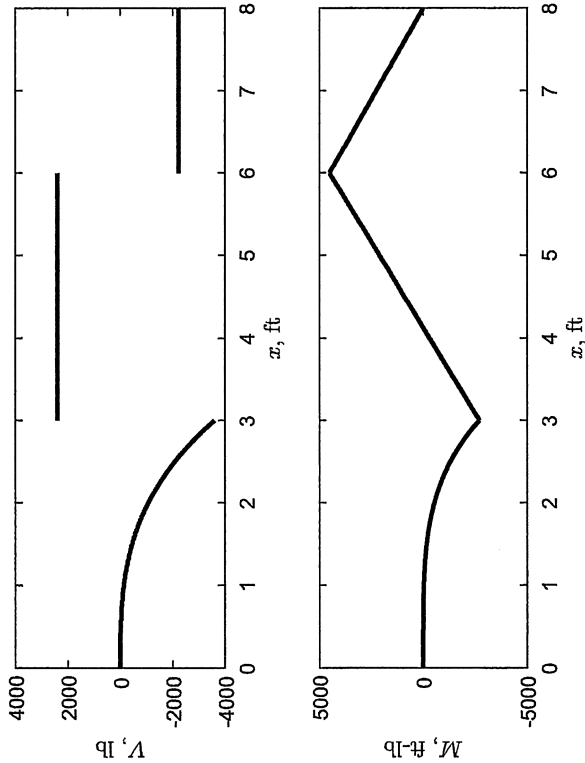
$M = 578$ in-lb at $x = 9.33$ in.

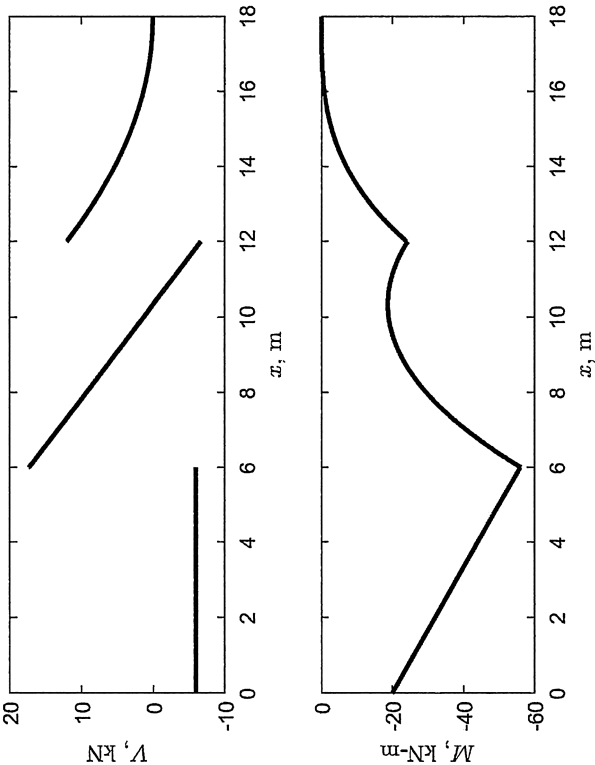
5.36



(continued)

5.38

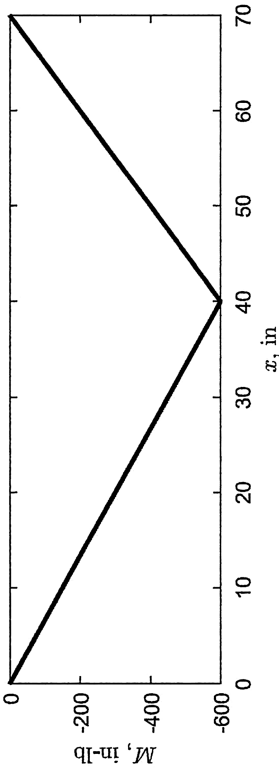
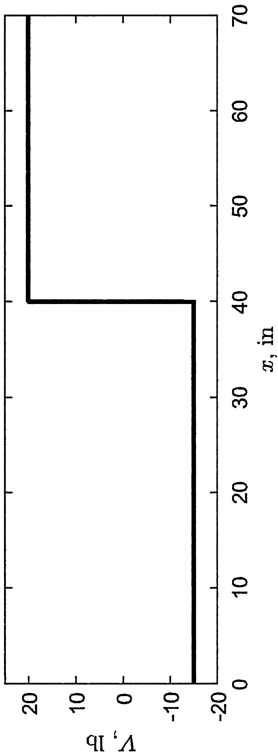


5.40	
5.42	$V = -31.3 + 10x + 0.25x^2 - 0.2x^3$ kN.
5.44	$V = -w_0(x - x^2/2L)$, $M = -w_0(x^2/2 - x^3/6L)$.
5.46	$V = F$, $M = Fx$.
5.48	$V = w_0L/6 - w_0x^2/2L$, $M = (Lx - x^3/L)w_0/6$.
5.50	$V = w(L/2 - x)$, $M = -(w/2)(L^2/6 - Lx + x^2)$.
5.54	$0 < x < 2$ m: $P = 0$, $V = x$ kN, $M = x^2/2$ kN-m. $2 < x < 5$ m: $P = 0$, $V = -4 + x$ kN, $M = 8 - 4x + x^2/2$ kN-m. $5 < x < 6$ m: $P = 0$, $V = -6 + x$ kN, $M = 18 - 6x + x^2/2$ kN-m.

(continued)

5.58

(a) $V = -15\langle x \rangle^0 + 35\langle x - 40 \text{ in} \rangle^0 - 20\langle x - 70 \text{ in} \rangle^0 \text{ lb}$,
 $M = -15\langle x \rangle + 35\langle x - 40 \text{ in} \rangle - 20\langle x - 70 \text{ in} \rangle \text{ in}\cdot\text{lb}$.
(b)

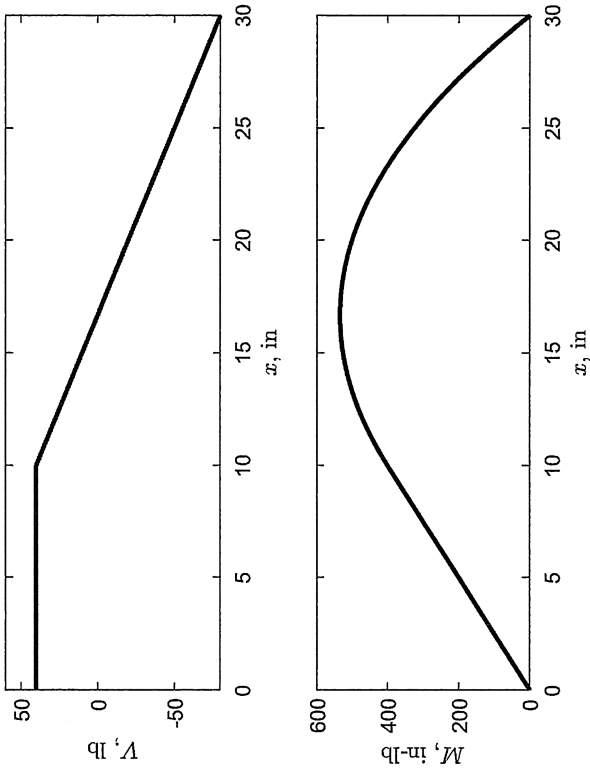


5.60

$V = 2F\langle x \rangle^0 - F\langle x - \frac{L}{3} \rangle^0 - 4F\langle x - \frac{2L}{3} \rangle^0 + 3F\langle x - L \rangle^0$,
 $M = 2F\langle x \rangle - F\langle x - \frac{L}{3} \rangle - 4F\langle x - \frac{2L}{3} \rangle + 3F\langle x - L \rangle$.

5.62

(a) $V = 40\langle x \rangle^0 - 6\langle x - 10 \text{ in} \rangle + 80\langle x - 30 \text{ in} \rangle^0 \text{ lb}$,
 $M = 40\langle x \rangle - 3\langle x - 10 \text{ in} \rangle^2 + 80\langle x - 30 \text{ in} \rangle \text{ in}\cdot\text{lb}$.
(b)

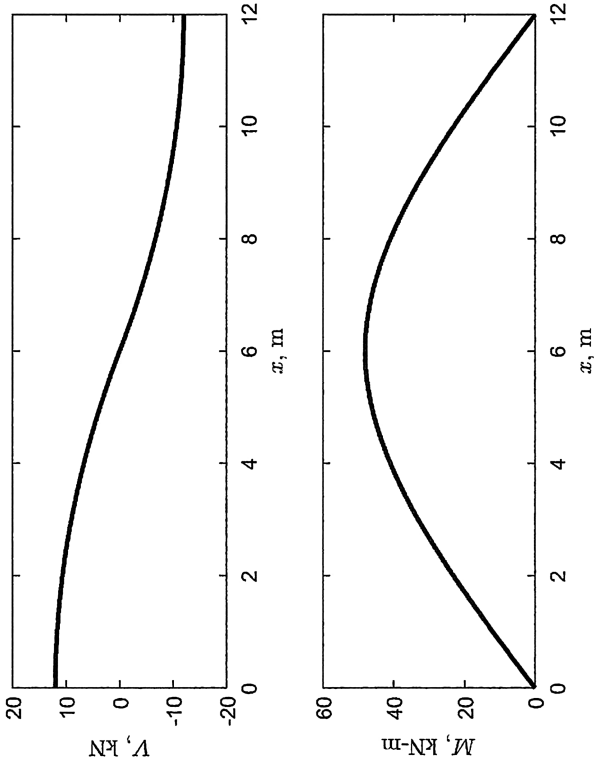


(continued)

5.64

(a) $V = 12\langle x \rangle^0 + 12\langle x - 12 \text{ m} \rangle^0 - \frac{1}{3}\langle x \rangle^2 + \frac{2}{3}\langle x - 6 \text{ m} \rangle^2 \text{ kN},$
 $M = 12\langle x \rangle + 12\langle x - 12 \text{ m} \rangle - \frac{1}{9}\langle x \rangle^3 + \frac{2}{9}\langle x - 6 \text{ m} \rangle^3 \text{ kN}\cdot\text{m}.$

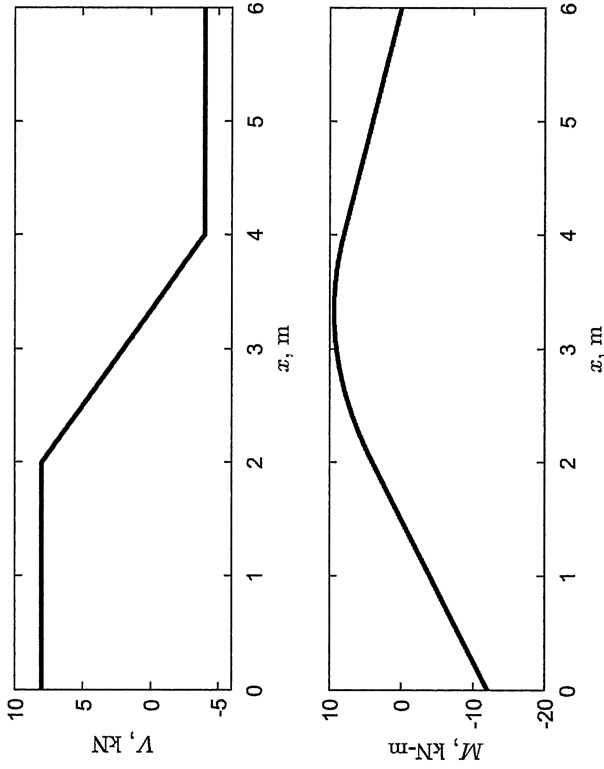
(b)



5.66

(a) $V = -12\langle x \rangle^{-1} + 8\langle x \rangle^0 + 4\langle x - 6 \text{ m} \rangle^0 - 6\langle x - 2 \text{ m} \rangle + 6\langle x - 4 \text{ m} \rangle$ kN,
 $M = -12\langle x \rangle^0 + 8\langle x \rangle + 4\langle x - 6 \text{ m} \rangle - 3\langle x - 2 \text{ m} \rangle^2 + 3\langle x - 4 \text{ m} \rangle^2$ kN·m.

(b)



5.68

$P_C = 0$, $V_C = -2$ kN, $M_C = -4$ kN·m.

5.70

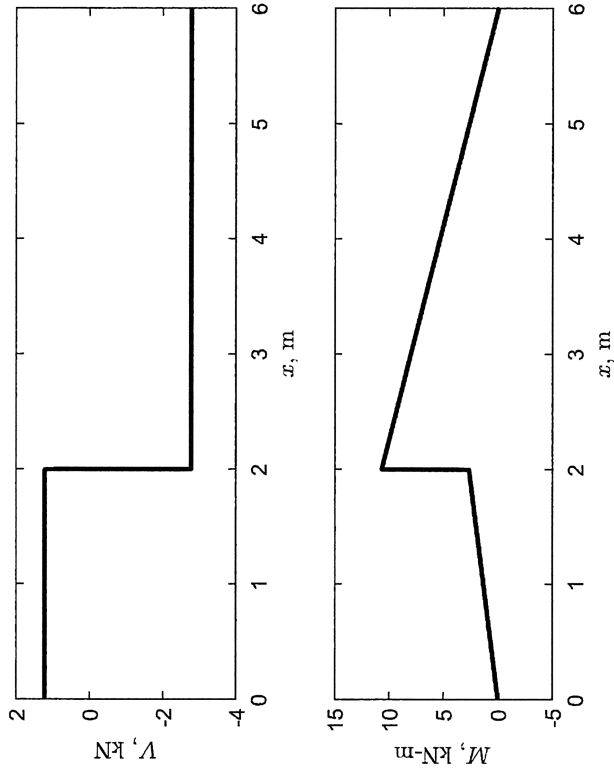
$P_A = 0$, $V_A = 225$ kN, $M_A = -375$ kN·m.

5.72

No. The resulting maximum bending moment magnitude is 8 kN·m

(continued)

5.74



6.2 (a) $\sigma_x = -9380$ psi. (b) 18, 800 psi.

6.4 $M = 492$ kN-m.

6.6 $M = 177,000$ in-lb.

6.8 (a) $M = 22.1$ N-m. (b) $\sigma_{\max} = 8.28$ MPa.

6.10 (a) $\sigma_x = 129$ MPa. (b) $\sigma_x = 78.6$ MPa.

6.12 (a) $M = 2700$ N-m at $x = 2.25$ m. (b) 11.8 MPa.

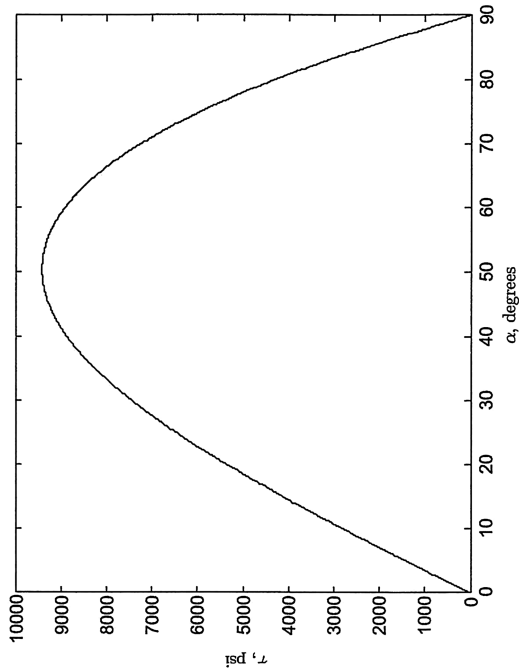
6.14 (a) $\sigma_x = 13.1$ ksi. (b) $\sigma_x = 6.75$ ksi.

6.16	$\sigma_x = 1.24 \text{ GPa.}$
6.18	$FS = 1.87.$
6.20	$h = 3.90 \text{ in.}$
6.22	(a) $FS = 2.01.$ (b) $FS = 4.69.$
6.28	W150X29.8
6.30	W6X16
6.32	Steel, 1520 psi; aluminum, 876 psi
6.34	$H = 0.02 \text{ m.}$
6.36	$H = 2.8 \text{ in.}$
6.38	$E_B = 216 \text{ GPa.}$
6.40	(a) $\sigma_x = 26.3 \text{ MPa. (b)}$ $\sigma_x = 13.8 \text{ MPa.}$
6.42	(a) $w_0 = 1320 \text{ lb/in. (b)}$ $w_0 = 2580 \text{ lb/in.}$
6.44	$\sigma_x = 3.02 \text{ MPa.}$
6.46	$d = 0.0274 \text{ m.}$
6.48	(a) 640,000 in-lb. (b) 960,000 in-lb.
6.50	$w_0 = 50, 300 \text{ N/m.}$
6.52	$x = \sqrt{12} \text{ m, } d = 0.0293 \text{ m.}$
6.54	$w_0 = 22, 700 \text{ N/m, } x = 0.6 \text{ m.}$
6.56	$w_0 = 116 \text{ lb/in, } x = 18 \text{ in.}$
6.60	$M_U = 11.0 \text{ kN-m.}$
6.62	$\sigma_x = 31.3 \text{ MPa.}$
6.64	$\sigma_x = -14 \text{ MPa.}$
6.66	$ \sigma_x = 9210 \text{ psi.}$

(continued)

6.68	$ \sigma_x = 21,400 \text{ psi.}$
6.70	$ \sigma_x = 2.08 \text{ MPa.}$
6.72	$\sigma_x = -18,300 \text{ psi.}$
6.74	$\sigma_x = -48.6 \text{ MPa.}$
6.76	(a) $\tau_{av} = 4.44 \text{ MPa.}$ (b) $\tau_{av} = 2.78 \text{ MPa.}$
6.78	$\tau_{av} = 576 \text{ kPa}$ at $x = 0$, $y' = 0$ and at $x = 8 \text{ m}$, $y' = 0$.
6.80	(a) $\tau_{av} = -2810 \text{ psi.}$ (b) $\tau_{av} = -1230 \text{ psi.}$
6.84	$\tau_{av} = 6.86 \text{ MPa.}$
6.86	$y' = 1 \text{ in.}$, $\tau_{av} = 4170 \text{ psi.}$
6.88	$\tau_{av} = 11.4 \text{ MPa.}$
6.90	$\tau_{av} = 6.31 \text{ MPa.}$
6.92	$\tau_{av} = 5.35 \text{ MPa.}$
6.94	3 kN/bolt
6.96	13.1 kN/bolt
6.98	577 N/bolt
6.100	$\tau = 30.9 \text{ MPa.}$
6.102	$\tau = 2250 \text{ psi.}$
6.104	$\tau = 138\zeta \text{ MPa}$ (ζ in meters)

6.106



6.108

$\tau = 2.65\alpha + 9,46 \sin \alpha$ MPa.

6.110

$e = 0,312$ m.

6.112

$e = 0,0332$ m.

6.114

$e = 7,54$ in.

6.116

$e = 0,0637$ m.

6.118

$e = 3,12$ in.

6.120

$e = 0,0394$ m.

6.122

$M = 16,000$ in-lb.

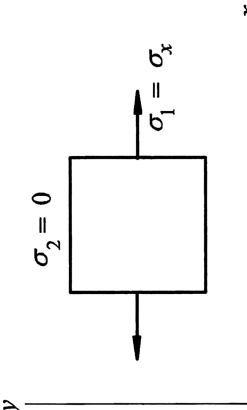
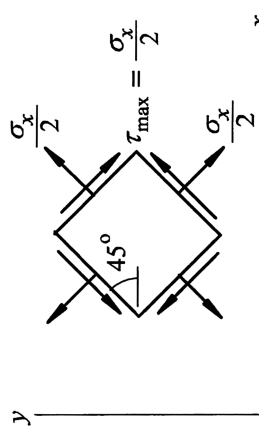
6.124

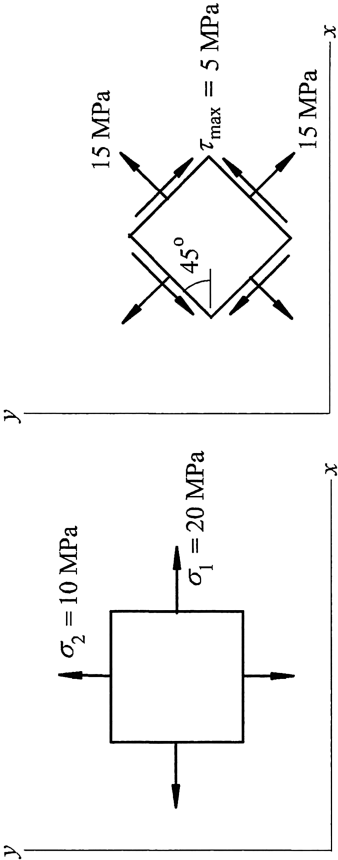
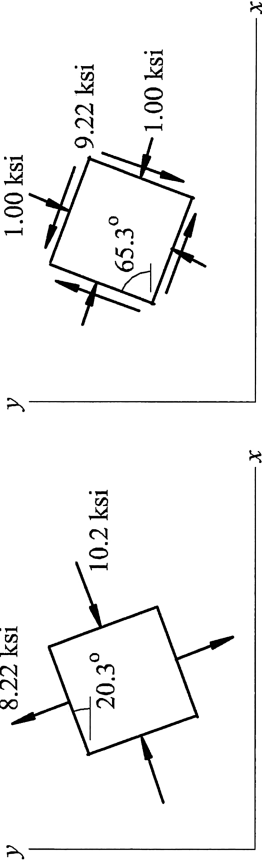
$6,84$ MPa.

6.126

$w_0 = 13,3$ kN/m.

(continued)

6.128	$w_0 = 9.32 \text{ kN/m.}$
6.130	$x = 2.86 \text{ m, } d = 50.7 \text{ mm.}$
6.132	$\sigma_x = -4.11 \text{ MPa.}$
6.134	(a) $\tau_{av} = -19.9 \text{ MPa. (b)}$ $\tau_{av} = -11.1 \text{ MPa.}$
6.136	$\tau_{av} = 223 \text{ psi.}$
7.2	(a) $\sigma_y = -4 \text{ MPa. (b)}$ $ \epsilon = 3.35 \text{ MPa.}$
7.4	(a) $\sigma_x = 360 \text{ psi, } \sigma_y = -480 \text{ psi, } \sigma_z = 0, \tau_{xy} = -640 \text{ psi, } \tau_{xz} = 0, \tau_{yz} = 0.$ (b) $\sigma_{x'} = -150 \text{ psi, } \sigma_{y'} = 29.6 \text{ psi, } \tau_{x'y'} = -760 \text{ psi.}$
7.6	$\sigma_{x'} = 25 \text{ ksi, } \sigma_{y'} = -25 \text{ ksi, } \tau_{x'y'} = 0.$
7.8	$\sigma_x = 64.00 \text{ MPa, } \sigma_y = 85.00 \text{ MPa, } \tau_{xy} = 0.00 \text{ MPa.}$
7.10	$\sigma_x = 38.8 \text{ MPa, } \sigma_y = -22.8 \text{ MPa, } \tau_{xy} = 14.3 \text{ MPa.}$
7.12	$\sigma = -2.23 \text{ ksi, } \tau = 1.60 \text{ ksi.}$
7.14	$\sigma_{(a)} = -56.6 \text{ MPa, } \sigma_{(b)} = -50.0 \text{ MPa, } \sigma_{(c)} = -33.2 \text{ MPa.}$
7.16	$\sigma = -7.86 \text{ MPa, } \tau = 13.50 \text{ MPa.}$
7.18	$\tau_{x'y'} = 4.90 \text{ MPa, } \theta = 19.5^\circ \text{ or } \tau_{x'y'} = -4.90 \text{ MPa, } \theta = 40.2^\circ.$
7.20	$\tau_{xy} = -78.4 \text{ psi, } \tau_{x'y'} = -114 \text{ psi.}$
7.24	$\sigma_1 = \sigma_x, \sigma_2 = 0, \tau_{\max} = \sigma_x/2 .$
<div><div></div><div></div></div>	

7.26	<p>$\sigma_1 = 20 \text{ MPa}$, $\sigma_2 = 10 \text{ MPa}$, $\tau_{\max} = 5 \text{ MPa}$.</p> 
7.28	<p>$\sigma_1 = 8.22 \text{ ksi}$, $\sigma_2 = -10.22 \text{ ksi}$, $\tau_{\max} = 9.22 \text{ ksi}$.</p> 
7.30	Absolute maximum shear stress = 10 MPa.
7.32	$\sigma_1 = 52.4 \text{ MPa}$, $\sigma_2 = -32.4 \text{ MPa}$, absolute maximum shear stress = 42.4 MPa.
7.36	No, the absolute maximum shear stress is 174 MPa
7.38	$\sigma_x = 25 \text{ ksi}$, $\sigma_y = -25 \text{ ksi}$, $\tau_{xy} = 0$.

(continued)

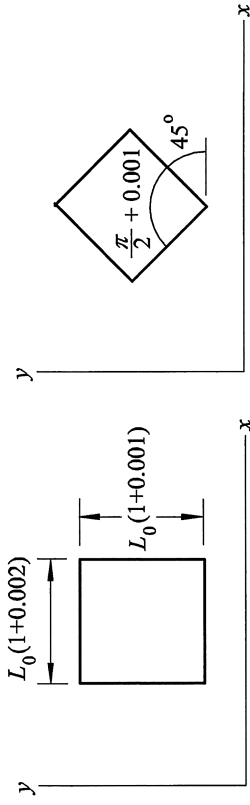
7.40	$\sigma_y = 64.0 \text{ MPa}$, $\sigma_y = 85.0 \text{ MPa}$, $\tau_{xy} = 0.00 \text{ MPa}$.
7.42	$\theta = -20^\circ$.
7.44	$\sigma = 5.8 \text{ MPa}$, $ \tau = 4.9 \text{ MPa}$.
7.46	$\sigma = 177 \text{ psi}$, $\tau = -237 \text{ psi}$.
7.48	See the answer to Problem 5–2.24
7.50	See the answer to Problem 5–2.26
7.52	$\sigma_1 = 52.5 \text{ MPa}$, $\sigma_2 = -32.5 \text{ MPa}$, $\tau_{\max} = 42.5 \text{ MPa}$.
7.54	Absolute maximum shear stress = 6.6 ksi .
7.56	$\sigma_1 = 40.5 \text{ ksi}$, $\sigma_2 = 0$, $\sigma_3 = -15.5 \text{ ksi}$, $\tau_{\text{abs}} = 28.0 \text{ ksi}$.
7.58	$\sigma_1 = 85.0 \text{ MPa}$, $\sigma_2 = 65.0 \text{ MPa}$, $\sigma_3 = 0$, $\tau_{\text{abs}} = 42.5 \text{ MPa}$.
7.60	$\sigma_1 = \sigma_2 = 240 \text{ MPa}$, $\sigma_3 = -120 \text{ MPa}$, $\tau_{\text{abs}} = 180 \text{ MPa}$.
7.62	$\sigma_1 = 409 \text{ ksi}$, $\sigma_2 = 148 \text{ ksi}$, $\sigma_3 = -257 \text{ ksi}$, $\tau_{\max} = 333 \text{ ksi}$.
7.64	(a), (b) $\sigma_1 = 8.22 \text{ ksi}$, $\sigma_2 = 0$, $\sigma_3 = -10.2 \text{ ksi}$.
7.68	$\sigma_1 = 46.4 \text{ MPa}$, $\sigma_2 = -7.42 \text{ MPa}$.
7.70	$\sigma_1 = 1700 \text{ psi}$, $\sigma_2 = -5890 \text{ psi}$, $\tau_{\max} = 3800 \text{ psi}$.
7.72	$T = 1.38 \text{ kN}\cdot\text{m}$.
7.74	$\sigma_1 = 2860 \text{ psi}$, $\sigma_2 = -318 \text{ psi}$, $\tau_{\max} = 1590 \text{ psi}$.
7.76	$\sigma_x = 1.11 \text{ MPa}$, $\sigma_y = 0$, $\tau_{xy} = 0$.
7.78	$F = 1235 \text{ N}$.
7.80	$\sigma = 142 \text{ ksi}$, $\tau_{\text{abs}} = 71.3 \text{ ksi}$.
7.82	$\sigma_h = 250 \text{ MPa}$.
7.84	$\sigma_h = 15 \text{ MPa}$, $\tau_{\text{abs}} = 7.65 \text{ MPa}$.
7.86	$t = 6.02 \text{ mm}$.
7.92	$\sigma = 7.10 \text{ MPa}$, $ \tau = 1.57 \text{ MPa}$.
7.94	$\mathbf{t} = 2.67 \mathbf{i} - 0.332 \mathbf{j} + 3.00 \mathbf{k} \text{ (ksi)}$.
7.96	$\sigma = 6.86 \text{ GPa}$, $ \tau = 2.15 \text{ GPa}$.
7.98	$ \tau = 10.0 \text{ MPa}$.
7.100	$\sigma = \sigma_1$, $ \tau = 0$.

7.102	$\sigma = -353 \text{ psi}, \tau = 44.5 \text{ psi}.$
7.106	$\theta = -20.0^\circ.$
7.108	$\sigma = -353 \text{ psi}, \tau = -44.5 \text{ psi}.$
7.110	Absolute maximum shear stress = 6.54 ksi.
7.112	$\sigma = 3530 \text{ psi}, \tau = 1290 \text{ psi}.$
7.114	$\tau_{\text{abs}} = 250 \text{ MPa}.$
7.116	$\sigma_x = 13.5 \text{ MPa}, \sigma_y = 0, \tau_{xy} = 4.77 \text{ MPa}.$
7.118	$\sigma_x = 375 \text{ psi}, \sigma_y = 0, \tau_{xy} = 0.$
7.120	2.11E5 Pa.
8.2	$\epsilon_x = -0.004, \epsilon_z = 0.0015, \gamma_{xz} = 0.00244.$
8.4	$\gamma_{xy} = 0.000997.$
8.6	$\theta = -20.0^\circ.$
8.8	$\epsilon_x = 0.00640, \epsilon_y = 0.00850, \gamma_{xy} = 0.$
8.10	$\gamma_{x'y'} = 0.0098, \theta = 19.5^\circ$ or $\gamma_{x'y'} = -0.0098, \theta = 40.2^\circ.$
8.12	$PQ = 0.997 \text{ mm}.$
8.14	$\gamma_{xy} = -0.00360.$
8.16	$\epsilon_x = -0.00201, \epsilon_y = 0.00811, \gamma_{xy} = -0.00250.$
8.18	1.57626 rad (90.313°)
8.20	$\epsilon_a = 0.00232, \epsilon_b = 0.00203, \epsilon_c = 0.00475.$
8.22	$\epsilon_x = 0.003, \epsilon_y = -0.001, \gamma_{xy} = 0.$
8.24	$\epsilon_d = -0.00605.$

(continued)

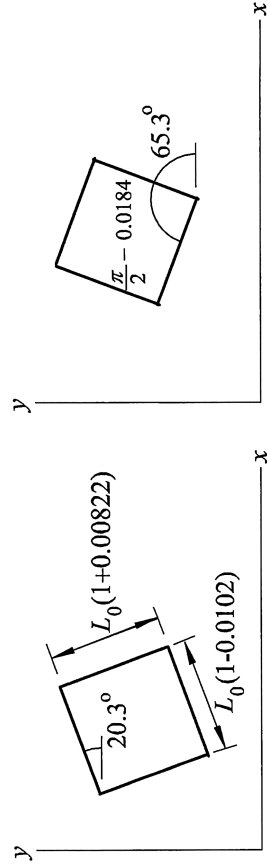
8.26

$\epsilon_1 = 0.002, \epsilon_2 = 0.001, \gamma_{\max} = 0.001.$



8.28

$\epsilon_1 = 0.00822, \epsilon_2 = -0.01022, \gamma_{\max} = 0.01844.$



8.30

$\epsilon_1 = 0.00472, \epsilon_2 = -0.00272, \gamma_{\max} = 0.00743.$

8.32

Absolute maximum shear strain = 0.00314.

8.38

$\epsilon_{x'} = 0.002, \epsilon_{y'} = -0.002, \gamma_{x'y'} = 0.$

8.42

$\gamma_{x'y'} = 0.00255, \theta = 14^\circ$ or $\gamma_{x'y'} = -0.00255, \theta = 40^\circ.$

8.44

$\epsilon_x = 0.0039, \epsilon_y = -0.0059, \gamma_{xy} = 0.012.$

8.46

See the answer to Problem 8.26

8.48

See the answer to Problem 8.28

8.50	$\epsilon_1 = 0.00368, \epsilon_2 = -0.00608, \gamma_{\max} = 0.00977.$
8.52	$\sigma_x = 42.5 \text{ MPa}, \sigma_y = -37.2 \text{ MPa}, \sigma_z = -26.4 \text{ MPa},$ $\tau_{xy} = 19.4 \text{ MPa}, \tau_{yz} = -12.9 \text{ MPa}, \tau_{xz} = 10.8 \text{ MPa}.$
8.54	The required condition is that $\sigma_x + \sigma_y = 0.$
8.56	$\sigma_x = 63.8 \text{ ksi}, \sigma_y = 83.3 \text{ ksi}, \tau_{xy} = -93.6 \text{ ksi}.$
8.58	(a) $\lambda = 46.2 \text{ GPa}, \mu = 30.8 \text{ GPa}.$ (b) $K = 66.7 \text{ GPa}.$
8.60	$\sigma_x = 34.2 \text{ ksi}, \sigma_y = -33.5 \text{ ksi}, \sigma_z = -44.8 \text{ ksi},$ $\tau_{xy} = 56.4 \text{ ksi}, \tau_{yz} = 0, \tau_{xz} = -56.4 \text{ ksi}.$
8.62	(a) $\epsilon_x = \sigma_x/E, \epsilon_y = \epsilon_z = -\nu\sigma_x/E,$ other strain components equal zero. (b) Volume $= (1 + \sigma_x/E)(1 - \nu\sigma_x/E)^2 LA.$
8.64	$\sigma_x = -55.5 \text{ MPa}, \sigma_y = 104 \text{ MPa}, \tau_{xy} = -94.3 \text{ MPa}.$
8.66	$\sigma_x = 413 \text{ MPa}, \sigma_y = 444 \text{ MPa}, \tau_{xy} = -74.5 \text{ MPa}.$
8.68	$\epsilon_x' = 0.002, \epsilon_y' = -0.002, \gamma_{x'y'} = 0.$
8.70	$\epsilon_x = 0.00360, \epsilon_y = 0.00320, \gamma_{xy} = -0.00358.$
8.72	$\epsilon_x = -0.00160, \epsilon_y = 0.00100, \gamma_{xy} = 0.00201.$
8.74	Absolute maximum shear strain $= 0.00559.$
8.76	$\sigma_x = -253 \text{ MPa}, \sigma_y = 809 \text{ MPa}, \tau_{xy} = -234 \text{ MPa}.$
9.2	$ v = 3.03 \text{ mm}.$
9.4	$w = 19.3 \text{ lb/in}.$
9.6	Displacement magnitude is 10.4 mm, slope is zero
9.8	$v = -0.558 \text{ in}, v' = -0.0106 \text{ rad}.$
9.10	$ v = 28.2 \text{ mm}.$
9.22	$\sigma_x = 5.04 \text{ MPa}.$
9.24	$ v = 3.02 \text{ mm}$ at $x = 1.63 \text{ m}.$
9.26	$M_0 = 98.2 \text{ kN-m}.$
9.28	$x = 36.4 \text{ in}.$
9.30	$A_x = 0, A_y = -3M_0/(2L), M_A = M_0/2$ clockwise, $B = 3M_0/(2L).$
9.32	$A_x = 0, A_y = 9w_0 L/40, M_A = 7w_0 L^2/120$ counterclockwise, $B_y = 11w_0 L/40.$

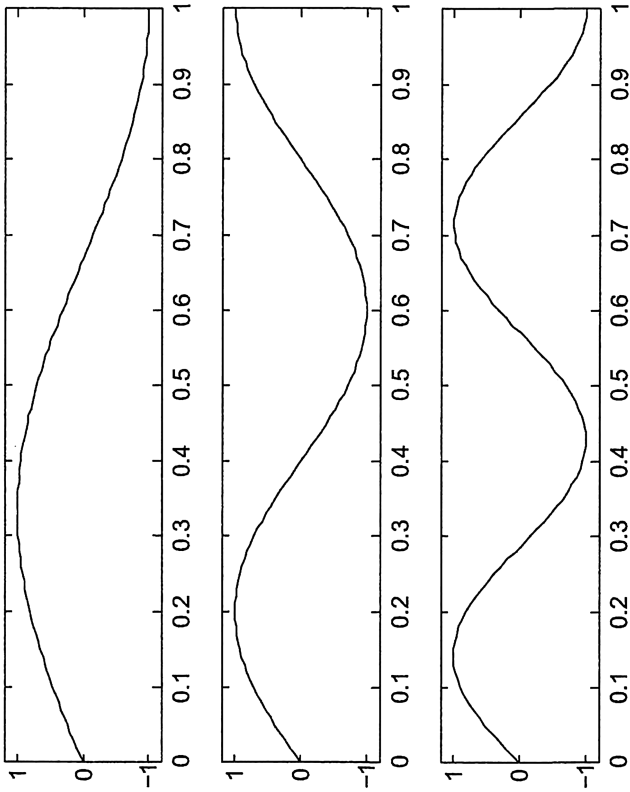
(continued)

9.34	$F_0 = 12, 200 \text{ lb}, M_0 = 294, 000 \text{ in}\cdot\text{lb}.$
9.36	$x = 30.4 \text{ in and } 114 \text{ in}.$
9.38	$w_0 = 38.1 \text{ kN/m}.$
9.40	$v = -w_0 L^4 / (768EI).$
9.42	$v = 27.1 \text{ mm}.$
9.44	$A = 2295 \text{ lb}, M_A = 91, 800 \text{ in}\cdot\text{lb}$ counterclockwise.
9.46	$v = -(w_0/384EI)(16x^4 - 38Lx^3 + 29L^2x^2 - 8L^3x + L^4).$
9.48	$v = (M_0/24LEI)[4\langle x \rangle^3 - 12L\langle x - L/2 \rangle^2 - 4\langle x - L \rangle^3 - L^2\langle x \rangle].$
9.50	$v = -10.1 \text{ mm}.$
9.52	$v = -20.0 \text{ mm}.$
9.54	$F = 3.83 \text{ kN}.$
9.56	$v_B = -M_0 L^2 / 2EI.$
9.58	$v_B = -w_0 L^4 / 8EI.$
9.60	$v_B = -6.22 \text{ mm}.$
9.62	$v = -(Fx^2/6EI)(3L - x) + M_0 x^2 / 2EI.$
9.64	$v = -(w_0 x / 24EI)(L^3 - 2Lx^2 + x^3) + (Fx/48EI)(3L^2 - 4x^2).$
9.66	$A = C = 1.5 \text{ kN}, B = 5 \text{ kN}.$
9.68	$v = -0.225 \text{ in}.$
9.70	$v = -w_0 L^4 / (384EI).$
9.72	$B = 2.71 \text{ kN}, C = 1.71 \text{ kN}.$
9.76	$A_x = 0, A_y = 11F/16, M_A = 3LF/16$ counterclockwise, $B_y = 5F/16.$
9.78	$v = -0.007L^3 F / (EI).$
9.80	$ M_0 = 72, 700 \text{ in}\cdot\text{lb}.$

9.82	$v = -66.6 \text{ mm.}$
10.2	$P = 965 \text{ kip.}$
10.4	$P = 202 \text{ kN.}$
10.6	$P = 806 \text{ kN.}$
10.10	$R = 21.5 \text{ mm.}$
10.12	$F = 80.4 \text{ kip.}$
10.14	$F = 3.02 \text{ kN.}$
10.16	$m = 250 \text{ kg.}$
10.18	$b = 3.10 \text{ in, } F = 5.66 \text{ kip.}$
10.20	$R_{AB} = 28.0 \text{ mm, } R_{CD} = 0.798 \text{ mm.}$
10.22	$F = 368 \text{ N.}$
10.24	$F = 3.18 \text{ kN.}$
10.26	$P = 1.25 \text{ MN.}$
10.28	$P = 31.7 \text{ kip.}$
10.30	$P = 588 \text{ kN.}$
10.32	$P = 7.20 \text{ MN. It bends in the } x\text{-}y \text{ plane}$
10.34	$P = 1.66 \text{ MN. It bends in the } x\text{-}y \text{ plane}$

(continued)

10.36



10.38

$P = \pi^2 EI / L^2.$

10.40

$L_c = L, L/2, L/3, \text{ and } L/4; K = 1, 1/2, 1/3, \text{ and } 1/4.$

10.42

$L_c = 2L, P = \pi^2 EI / 4L^2.$

10.44

$v_{\max} = 0.0102 \text{ m.}$

10.46

$v_{\max} = 0.781 \text{ in.}$

10.48

$v_{\max} = 0.738 \text{ mm.}$

10.50

$v_{\max} = 6.68 \text{ mm.}$

10.52	$P = 264 \text{ kN}.$
10.56	$P = 6.70 \text{ MN}.$
10.58	$R_1 = 15.5 \text{ mm}.$
10.60	$h/b = 2.86.$
10.62	$\sigma_{\max} = 161 \text{ MPa}.$
11.2	(a) $U = 0.00167 \text{ J}$ (joules, or N-m). (b) $W = 0.00167 \text{ J}.$
11.4	(a) $U = 386 \text{ in-lb}.$ (b) $W = 386 \text{ in-lb}.$
11.6	$\theta = 0.00321 \text{ rad}$ (0.184°) counterclockwise
11.8	$F = 98.6 \text{ kN}.$
11.10	$v = (1 + 2\sqrt{2})FL_0/(EA).$
11.12	$v = 0.833 \text{ in}.$
11.14	$v = FL^3/12EI.$
11.16	$u = 1.24 \text{ MJ/m}^3.$
11.20	$v = 0.0977 \text{ in}.$
11.22	$\theta_B = w_0L^3/6EI.$
11.24	$v_B = M_0L^2/2EI.$
11.26	$v = FL^3/12EI.$
11.28	$3M_0/2L$ upward.
11.30	$v = 0.257 \text{ in}.$
11.32	$v = 11.1 \text{ mm}.$
12.2	$W = 6 \text{ in}.$
12.4	Spacing is satisfactory
12.6	$C = 1.35.$
12.8	$d_2 = 1.0 \text{ in}.$
12.10	Naval brass, hard
12.12	$a = 0.0855 \text{ in}.$
12.14	$10.2 \text{ MW}.$

(continued)

12.16	$W = 500 \text{ kN}$.
12.18	Case (a).
12.20	$M = 50.7 \text{ kN}\cdot\text{m}$.
12.22	$a = 0.137 \text{ m}$, $C = 1.4$.
12.24	$M = 23.7 \text{ kN}\cdot\text{m}$.
12.26	It will fail
12.28	It will suffice
12.30	No
12.32	15% increase
12.34	$FS_T = 1.20$.
12.36	$R = \left[\frac{10}{\pi \sigma_Y} \sqrt{M^2 + T^2} \right]^{1/3}$.
12.38	$FS_M = 13.1$.
12.40	$\tau_{xy} = 120 \text{ MPa}$ or $\tau_{xy} = -120 \text{ MPa}$.
12.42	3320 cycles
12.44	Damage is 0.036, 0.376, and 0.520, 9.561E3 cycles
12.46	15.2 years
12.48	33, 800 cycles.
12.50	5.34 years
12.52	$\sigma = 6.76 \text{ ksi}$.
12.54	(a) $\sigma = 17.4 \text{ ksi}$. (b) $\sigma = 35.0 \text{ ksi}$. (c) $\sigma = 47 \text{ ksi}$.
12.56	$h = 0.5 \text{ m}$.
12.58	Yes, the plate will fail
12.60	Yes, it will
12.62	$a = 0.221 \text{ in}$.
12.64	$c_0 = 28.6 \text{ mm}$. It is satisfied.
12.66	936 kilocycles.
12.68	$W = 2040 \text{ lb}$.

12.70	(a) Yes. (b) Yes. (c) 650 kilocycles.
C.2	$\bar{x} = a(n+1)/(n+2), \bar{y} = ca^n(n+1)/(4n+2).$
C.4	$\bar{x} = 0, \bar{y} = 1.6 \text{ ft.}$
C.6	$\bar{x} = 0.5, \bar{y} = -7.6.$
C.8	$\bar{x} = \bar{y} = 4R/(3\pi).$
C.10	$\bar{x} = 70.9 \text{ mm}, \bar{y} = 0.$
C.12	$\bar{x} = 12.0 \text{ in}, \bar{y} = 5.49 \text{ in.}$
C.14	$\bar{x} = 344 \text{ mm}, \bar{y} = 456 \text{ mm.}$
C.16	$I_x = \frac{1}{12}bh^3, I_y = \frac{1}{12}hb^3, I_{xy} = \frac{1}{24}b^2h^2.$
C.18	$I_x = I_y = \frac{1}{16}\pi R^4, I_{xy} = \frac{1}{8}R^4.$
C.20	$I_x = 2.65\text{E}8 \text{ mm}^4.$
C.22	$I_{xy} = 92.3 \text{ ft}^4.$
C.24	$I_x = 237 \text{ in}^4, I_y = 115 \text{ in}^4, I_{xy} = 119 \text{ in}^4.$
C.26	$I_x = 88.8 \text{ m}^4, I_y = 65 \text{ m}^4.$
C.28	$\theta_p = 0, I_{x'} = 85.33 \text{ m}^4, I_{y'} = 5.33 \text{ m}^4.$
C.30	$\theta_p = 35.6^\circ, I_{x'} = 1.02\text{E}5 \text{ m}^4, I_{y'} = 1.12\text{E}6 \text{ m}^4.$
C.32	$\theta_p = 26.6^\circ, I_{x'} = 10 \text{ ft}^4, I_{y'} = 2.5 \text{ ft}^4.$